THE FUNDAMENTALS OF LAYING OUT A SWITCHING-REG-ULATOR BOARD CAN BE USEFUL WHEN YOU'RE WORKING WITH ALL TYPES OF SWITCHING REGULATORS, INCLUDING A STEP-UP SWITCHING REGULATOR.

Basic switching-regulatorlayout techniques

HEN CONSIDERING HOW BEST to lay out a switching-regulator board, it's good to recall its purpose, which is to supply a steady voltage of a specific magnitude. Experienced layout designers achieve that steady voltage by paying close attention to the grounding scheme; they assume that ground is never perfect—in other words, that ground is not just ground, and what you do with it is crucial to the success of the circuit. Also, they pay particular attention to where they place the various regulator components.

It is perhaps a mistake to let undergraduate engineers draw the three small lines that represent ground. That symbol tends to foster the fantasy that ground is ideal. By instead drawing longer lines that connect the various circuit components to a power supply's or a battery's negative terminal, you more readily intuit that ground is flawed. Those lines suggest that currents flow back to the power source through the resistance and inductance of a ground plane or trace, creating voltage drops in the process. Thus, they quietly point out that ground varies from

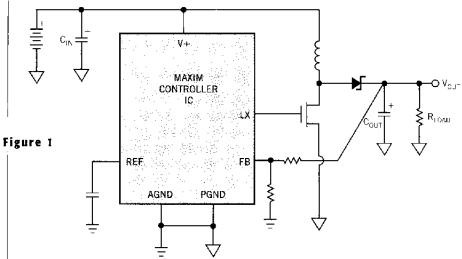
the perfectly steady voltage that you typically call 0V.

The boost converter of Figure 1 illustrates why it's necessary to account for imperfect grounds. This regulator relies on both the reference within the controller IC and the two feedback resistors to generate a specific voltage. To obtain accurate feedback and therefore an accurate output, the grounds of the reference, the resistor divider, and the output capacitor must reside at the same potential. More specifically, the voltage of the controller's analog ground pin, which is the reference's ground, and the voltage of the resistor divider's ground terminal must equal the voltage of the output capacitor's ground terminal. The output capacitor's ground-terminal voltage is important, because you usually place the load, which is what requires the regulator's accurate output voltage, next to the output capacitor. Thus, you want the feedback to be referred to that part of ground.

The circuit must feed back an accurate voltage to the controller for another reason. To achieve jitterfree switching, the controller requires an accurate picture of any ac perturbations of the output voltage. It receives that accurate picture via the feedback.

COMPONENT PLACEMENT

In addition to the grounding scheme, proper placement of the regulator's components is important. For example, you must bypass the reference within the controller by placing a capacitor close to the REF pin; noise on the reference could affect the output voltage. Also, this bypass capacitor's ground terminal must connect to a quiet ground (along with the controller's analog ground pin and the resistor divider's ground terminal). Further, it is important



The ideas behind a successful board layout for this step-up switching regulator also apply to the layout of other switching-regulator topologies.

to isolate this quiet ground from the noisier power ground.

Why must you isolate the noisier ground from the quieter one? After all, you'll have to connect the grounds of the two sections together, anyway. Such isolation is necessary to prevent high-level switching currents from returning to the battery or the supply through the same ground-return path as the analog signals, which disturbs the ground path of those sensitive signals. The high-level switching currents flowing through the ground's resistance and inductance will cause the voltage along the return path to vary.

A look at the noisier power section can show you how best to isolate it from the rest of the circuit. Figure 2 depicts the two current pathways of the regulator's power section. When the MOSFET is on, current flows through the input loop; when it's off, current flows through the output loop. By placing the components that make up each of the two loops close to each other, the high currents remain in the regulator's power section (and out of the ground-return path of the quiet components). So C_{IN}, L₁, and Q1 should be close to each other. C_{DC} , L_{1} , D_{1} , and C_{OCT} should also be close. The somewhat un-

together.

An actual layout usually involves some compromise. And compromise could be necessary when laying out the components of the two loops mentioned above. If you're unable to place close together all the components that you've decided should be close together, then you should determine which components in each loop have discontinuous current flowing through them. Those components are the most important to position close to each other so as to minimize stray inductance (see section "Minimize stray capacitance, inductance," below).

usual shapes of the two loops in Figure

2 clarify which components belong close

OTHER CONSIDERATIONS

Regardless of whether a battery or a power supply powers the step-up switch-

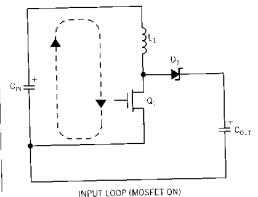
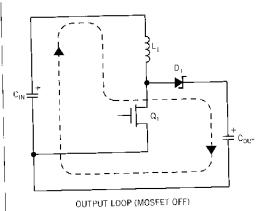


Figure 2



You must take special care to place the components of each of the two current loops close together. Using short, wide traces to achieve this tight layout improves efficiency, reduces ringing, and helps prevent interference to quieter parts of the circuit.

ing regulator, the power source exhibits a nonzero resistance. Therefore, as the regulator draws quickly changing current from the power source, the power source's voltage varies. To ameliorate that effect, board designers place the input bypass capacitors near the two power loops described above. (Sometimes, they use two capacitors: a ceramic capacitor and a polarized capacitor, in parallel.) They take this step not to steady the voltage fed to the power section; the power section will still function well if the voltage feeding it varies. Rather, placing the bypass capacitor near the power loops helps confine high ac currents to the power section, which helps keep those currents from interfering with quieter circuitry.

How might that interference occur? Three ways. First, as mentioned above, if the power section's ground-return current flows through part or all of the ground-return path of some sensitive portion of the regulator's analog circuitry, it would add switching noise to that ground path due to the resistance and inductance within it. That ground noise would degrade the accuracy of the regulator's output. It could also disturb other sensitive circuits that reside on the same board. Second, similar to concerns about the ground path, switching noise on the battery's or the power supply's positive rail can be conducted to other components that the same rail powers, including the controller IC, whose reference could bounce. Adding an RC filter at the controller's supply pin can help if the voltage across the input bypass capacitor varies. Third, the larger the area over which ac currents flow, the larger the magnetic field they create, and, hence, the greater the chance that those currents will cause interference. Placing the input bypass capacitor next to the power section minimizes that area and thus the potential interference.

Noise can also cause problems if you improperly place the two divider resistors. Placing the two resistors next to the controller's FB pin ensures that the circuit feeds back to the controller a relatively noise-free voltage. Positioning the resistors in this way minimizes the length of the trace leading from the midpoint of the resistor divider to the switching regu-

lator's FB pin-a necessity, because both the resistor divider and the input of the internal comparator at the FB pin are high impedances. Thus, the trace connecting them is prone to picking up (primarily through capacitive coupling) the noise that switching regulators inevitably produce. You can, however, make the trace that runs from the regulator's output to the "top" of the resistor divider and the trace that runs from the "bottom" or ground side of the resistor divider to the ground side of the output capacitor relatively long; the low output impedance of the switching regulator reduces coupled noise on those traces.

MINIMIZE STRAY CAPACITANCE, INDUCTANCE

Identifying nodes in the Figure 1 circuit where voltage quickly changes indicates where to minimize capacitance, because a capacitor's voltage prefers not to

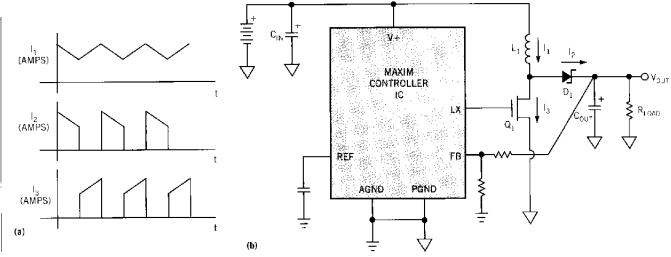


Figure 3 The current waveforms (a) of the branches of the switching-regulator circuit (b) indicate where to minimize stray inductance. Quickly changing currents (I, and I,, for example) requires you to minimize inductance in their paths.

change quickly. The node formed by the junction of the inductor, diode, and MOSFET is the only such point in the power portion of the circuit; it is near ground when the switch is on and rises to a diode drop above the output voltage when the switch is off. Make sure to run the board traces in a manner that minimizes the stray capacitance at this node. If stray capacitance slows the voltage transitions of this node, the regulator's efficiency will suffer. Keeping this node small not only helps reduce its stray capacitance, but also reduces the EMI that emanates from it. Don't make the area of the node small by using narrow traces, however. Instead, use wide, short traces.

Identifying circuit branches with quickly changing currents shows where to minimize inductance. Reminiscent of the voltage across a capacitor, the current through an inductor doesn't like to change quickly. When current through an inductance rapidly changes, it causes the voltage at that inductance to spike and ring, creating potential EMI problems. Also, the amplitude of that ringing voltage can be high enough to damage various circuit elements.

Figure 3 shows the current waveforms for the three branches of the circuit. Current I_1 presents no problem, because it changes in a relatively gradual manner; besides, a large inductance, L_1 , is already present there. However, inductance in series with the MOSFET can indeed cause a problem, because current I_3 changes abruptly. This series inductance includes inductance from anything within I_3 's return path up to C_{1N} 's ground terminal—

including stray inductance from Q_i 's leads as well as inductance in the ground-return path itself. Note that the current through $C_{\rm IN}$ undergoes no quick changes; it is equal to the ac portion of the inductor current (I_1) . (The battery supplies the dc portion.) A quickly changing current also flows through a portion of the loop formed when the MOSFET is off. This current, I_2 , flows through both D_1 and $C_{\rm OUT}$ as well as the copper in the ground-return path. Thus, you should minimize the stray inductance of those components and of that ground-return path.

When considering whether the inductance in the leads of the load also poses a problem, recall that if the output capacitor is large enough with a low enough ESR, its voltage remains relatively steady. That fact means that the current through the load resistor won't change much, and, therefore, the inductance in series with it doesn't matter—unless the load itself changes dynamically.

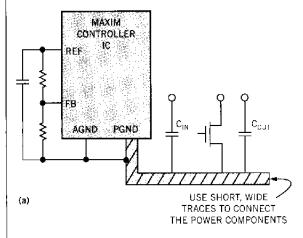
CREATING A FEASIBLE BOARD LAYOUT

There are a few ways to work with the ground portion of a switching-regulator circuit. One is to use a single ground plane for all ground connections—a method that probably won't work very well. When you use that technique, ground currents from the power portion of the circuit could pass through the same ground path as the ground current of the resistor divider, the capacitors used to bypass certain of the controller's pins, the controller's analog ground, or all three, causing their grounds to bounce.

Probably, the best approach is to create two separate ground sections: one for the power components and one for the more quiet analog portion of the regulator (Figure 4a). The ground portion of the power circuitry consists of the inputand output-capacitor ground terminals and the source of the MOSFET. You should make those connections with short, wide traces. Maximizing the width and minimizing the length of the power circuitry's ground traces (and of the other power traces) improve efficiency by reducing resistance.

The analog ground section provides a ground-return path for the controller's analog ground pin, the resistor-divider ground terminal, and the ground terminals of any capacitors that bypass certain controller pins (but not the main input bypass capacitor, $C_{\rm IN}$). The analog ground need not be a plane. Instead, you can use long, spread-out traces, because the currents are low-level and relatively constant; trace resistance and inductance aren't big factors.

Connect the controller's AGND pin to the PGND pin as shown in Figure 4a. Connecting the two ground sections at these pins ensures that no switching current circulates within the analog ground. The connection between AGND and PGND can be relatively narrow, because virtually no current flows via that path. Although the AGND pin would ideally connect directly to $C_{\rm OUT}$'s ground terminal, many controller ICs require that their two ground pins connect directly to each other. (Otherwise, problems can occur if the voltage between the two pins



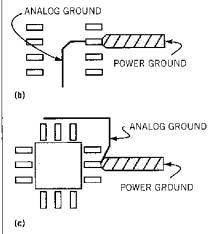


Figure 4 Using separate analogand power-ground

areas isolates the higher amplitude powerground currents from the quieter analog
ground currents, thus protecting the path
through which those quieter currents flow.
When the controller IC includes both an AGND
and a PGND pin, connecting the two ground
sections at those pins ensures that no switching
current circulates within the analog ground (a).
When the controller includes a single GND pin,
you can route the traces to prevent power current from mixing with sensitive analog current
(b). A third type of connection might be necessary if the controller's package includes a
grounded backside pad (c).

becomes large enough to turn on the diodes that are connected between them.) By making the trace from PGND to C_{OUT} short and wide, the feedback resistors and the reference inside the controller share essentially the same ground potential as the regulator's output. This fact is important, because these components are set up to control the output voltage.

Some controller ICs provide only one

ground pin. Figures 4b and 4c show how to lay out a board to accommodate such an arrangement.

Sometimes, capacitors bypass the controller, and you should not connect them to the analog or the power part of ground. An RC filter's bypassing the step-up switching regulator's V+ pin (as mentioned above) is one example. In that situation, the capacitor's ground pin

is too noisy for the analog ground; at the same time, the power ground is too noisy for the capacitor. You should return such a capacitor directly to the trace connecting the controller's AGND and PGND pins (or directly to the GND pin if the controller provides only one ground pin).

Finally, the number of board layers plays a part in a pc board's layout. On a multilayer board, you can use one of the inner layers as a shield. A shield layer allows you to place components on the opposite side of the board from noisy components with little chance of interference. When incorporating a shield layer, it's generally a bad idea to connect the ground-side leads of the power components through the shield. Instead, connect them in an isolated, confined area so that you know where those currents will flow and what effect they'll have.

Regardless of the number of layers, make those power-component ground connections on the top layer; doing so eliminates the need to use vias. If such a setup is impossible, you can make those connections through other layers using isolated copper pieces and vias. For each connection, use multiple vias in parallel to reduce their resistance and inductance...

AUTHOR'S BIOGRAPHY

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