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# Boost converter generates three analog rails 

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The standard boost converter in Figure 1 uses not only $\mathrm{IC}_{1}$, $\mathrm{C}_{1}, \mathrm{~L}_{1}, \mathrm{D}_{1}$, and $\mathrm{C}_{2}$ to generate a main 5 V output, but also additional small, low-cost components to provide two auxiliary supply rails of 10 and -5 V . These auxiliary outputs are useful for analog circuitry in small handheld instruments, which often require supply voltages greater than the signal range. Input voltages of 0.8 to 5.5 V , which is equivalent to voltages from a battery pack of one to three cells, sustain the main regulated output of $5 \mathrm{~V} \pm 2 \%$. With an input of 1.8 V from two flat cells, for instance, and with the other rails unloaded, the circuit can produce 25 mA with 80 to $90 \%$ efficiency.
The converter's LX switching node drives low-cost, discrete charge pumps via "flying capacitors" $\mathrm{C}_{3}$ and $\mathrm{C}_{6}$ to create the -5 V and 10 V outputs. The LX node switches between 0 V and a level-one diode drop above the 5 V rail, so the charge pumps' drive voltage is reasonably well-regulated. Moreover, the drop across $\mathrm{D}_{1}$ roughly compensates for diode drops in the two charge-pump outputs. IC $_{1}$ 's internal control scheme also assists in regulating the auxiliary outputs. This IC's current-limited, minimum-off-time, pulse-frequency modulation constantly adapts its switching frequency to the net load current; the frequency increases when the load increases, producing a greater transfer of energy via the flying capacitors. The result is a type of pseudoregulation for the charge-pump outputs.

These analog supply rails can drive precision op amps,
such as the MAX400 and OP-07, whose input common-mode-rejection and output-range specifications are 2 to 3 V within the supply rails. Thus, the rails are good enough if the -5 V output is less than -3 V and the 10 V output is more than 8V. Accordingly, the component choices in Figure 1, such as the lossy RC output filters and silicon signal diodes in place of Schottky diodes, provide for minimal cost and ripple rather than maximum regulation. The $4.7-\mu \mathrm{F}$ capacitors, $\mathrm{C}_{4}$ and $\mathrm{C}_{7}$, can be high-ESR, commodity, multilayerceramic types with 16 V ratings, a 1206 case, and a Y5V dielectric, such as the 1206YG475ZAT2A from AVX Corp (www.avxcorp.com).

The output ripple varies with the supply voltage and output load. Operating with an input voltage of 1.8 V , the circuit produces ripple amplitudes over the load of 2 to 10 mV p-p for the 10 V rail and 15 to 30 mV p-p for the -5 V rail. By increasing $\mathrm{C}_{5}$ and $\mathrm{C}_{8}$ to $2.2 \mu \mathrm{~F}$, you can reduce these ripple levels to 1 and 5 mV , respectively.

With no load on the auxiliary rails, the 5 V output's maximum available load current rises with input supply voltage (Figure 2a). You can increase this available output power by replacing $\mathrm{D}_{1}$ with a lower loss Schottky diode. At an input of 1.8 V , the output power available for the three rails (loaded with 10 mA at $5 \mathrm{~V}, 5 \mathrm{~mA}$ at 10 V , and 5 mA at -5 V ) is somewhat less than 125 mA ; with a $5-\mathrm{mA}$ load, the 10 V and -5 V outputs are approximately 9.75 and -3.7 V , respectively (Figure 2b ). A 2.7 V input based on three flat cells yields


Adding external charge pumps to this $\mathbf{5 V}$ boost converter produces auxiliary analog rails of 10 and $\mathbf{- 5 V}$.
around 275 mW .
The MAX858 operates with peak inductor currents of 125 mA . If you need more current, you can replace this IC with related parts that have 500 mA and 1 A ratings. Note that these changes require different passive components; the inductor and main output diode ratings must match the inductor's peak current. The charge pumps can remain the same if their output currents don't change much.

You can also retain the cheap, common, commodity dual diodes $\mathrm{D}_{1}, \mathrm{D}_{2}$, and $\mathrm{D}_{3}$, but detail specifications vary, so look carefully at data sheets for the part you actually use. For example, the BAV70's dc forward current, $\mathrm{I}_{\mathrm{F}}$, and peak forward surge current, $\mathrm{I}_{\mathrm{FSM}}$ for 1 $\mu s e c$, differ among manufacturers. For the Motorola (www.motorola.com) part, $\mathrm{I}_{\mathrm{F}}=200 \mathrm{~mA}$, and $\mathrm{I}_{\mathrm{FSM}}=500 \mathrm{~mA}$. For National Semiconductor (www. national.com), $\mathrm{I}_{\mathrm{F}}=600 \mathrm{~mA}$, and $\mathrm{I}_{\mathrm{FSM}}=2 \mathrm{~A}$. For Philips (www.philips.com), $\mathrm{I}_{\mathrm{F}}=125$ mA , and $\mathrm{I}_{\mathrm{FSM}}=4 \mathrm{~A}$, and for Vishay-Siliconix (www.siliconix.com), $\mathrm{I}_{\mathrm{F}}=250 \mathrm{~mA}$, and $\mathrm{I}_{\mathrm{FSM}}=4.5 \mathrm{~A}$. This caution is advisable in all second-source considerations. (DI \#2200)

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With auxiliary rails unloaded, the 5 V output's maximum available load current rises with input supply voltage (a). The auxiliary-output voltage levels depend on the load current (b).

