# 200 kHz 15W PUSH PULL DC-DC CONVERTER 

BY M. SUTERA

## INTRODUCTION

The 15 W DC-DC converter, shown in fig. 1 has a push-pull topology and works in continuous mode with two outputs ( $+6 \mathrm{~V},-6 \mathrm{~V}$ ) and features primary side control with full protection against fault conditions. There is no insulation between the primary
and secondary side.
Due to the high working frequency, the power switches used are the new SGS-THOMSON advanced POWER MOS type : IRFZ20 with high density and bonding on the active area.


The PWM controller is the linear integrated circuit SGS3525A, with dual source/sink output drivers, internal soft-start, pulse by pulse shut-down and ad-
justable dead-time control.
Table 1 shows the power supply specifications.

Table 1.

| Operating mode | $:$ | Push Pull |
| :--- | :--- | :--- |
| DC Input Voltage | $:$ | 10 V DC to 18 V DC |
| Switching Frequency | $:$ | $200 \mathrm{kHz} \pm 10 \%$ |
| Total Power Output | $:$ | 15 W |
| Outputs |  | $+6 \mathrm{~V} \pm 5 \% \quad 0.1$ to 1.3 A |
|  | $-6 \mathrm{~V} \pm 5 \% \quad 0.1$ to 1.3 A |  |
| Line Regulation (+6V output) | $0.05 \% / \mathrm{V}$ |  |
| Load Regulation (+6V output) | $:$ | $0.2 \% / \mathrm{A}$ |
| Efficiency (@1/2 load) | $:$ | $76 \%$ |
| Output Ripple @ Max Load $+6 \mathrm{~V},-6 \mathrm{~V}$ Outputs 50mV Peak to Peak |  |  |

Figure 1.


## CIRCUIT DESCRIPTION

The DC input is chopped at a high frequency ( 200 kHz ). This high switching frequency allows the use of a very small transformer.
Due to the push-pull configuration of the converter the POWER MOS devices, the transformer and the diodes work at the frequency of 100 kHz (photo 1,2) ; the output filters and the oscillator of PWM controller work at a frequency of 200 kHz (photo 3).
When Tr2 is on and Tr3 is off, diodes D2, D3 conduct and diodes D1, D4 are off. When Tr3 is on and Tr2 is off diodes D1, D4 conduct and diodes D2, D3 are off.

The snubber formed by C5, R17 is used to clamp the voltage spikes on Tr2 and Tr3 drains. With a leakage inductance $L_{d}=0.5 \mu \mathrm{H}$, a primary current $\mathrm{I}_{\mathrm{p}}=2.8 \mathrm{~A}$ at $\mathrm{V}_{\mathbb{N} M \operatorname{MIN}}$ and maximum load and an allowable voltage spike $V_{p}=30 \mathrm{~V}$ we can calculate C 5 as follows:
$\mathrm{C} 5=\frac{\mathrm{Ld}_{\mathrm{d}} \cdot \mathrm{l}_{\mathrm{p}}{ }^{2}}{\left(2 \mathrm{~V}_{\mathrm{MIN}}+\mathrm{V}_{\mathrm{p}}\right)^{2}-\left(2 \mathrm{~V}_{\mathrm{IN}}\right)^{2}}=1.8 \mathrm{nF}$
Eq. 1
The PWM controller SGS352A has the two drive outputs in totem-pole configuration in order to drive the POWER MOS. The feedback signal for the PWM is directly connected to the inverted input of
the error amplifier from the +6 V output by the resistive divider R4-R1. The maximum current protection is sensed by Tr1, R9, R8 and is connected to pin 10 (shut-down).
The magnetic coupling of the series inductance in the output filter is very important for good reguiation of the voltages. In this way when the load is very different in the two outputs $(+6 \mathrm{~V}$ max load ; -6 V min load or viceversa) the indirectly regulated output $(-6 \mathrm{~V})$ has a very stable output voltage (see fig. 2).

The efficiency is excellent : $70 \%$ over a wide range (fig. 3).
The transient response is very fast : about 50 ms . Photo 4 shows the transient response of load regulation due to a load variation from 100 mA to 1.3 A and from 1.3 A to 100 mA ( +6 V output).
Fig. 4 shows the P.C. board (track layout) and the component positions.

Figure 2.


Figure 3.


Figure 4 : P.C. Board and Components Layout (1:: 1 scale).


## TRANSFORMER

For this design a Tomita E core of 2E 6 ferrite material was chosen. To calculate the core size we used the following equations:

$$
A_{e} \cdot A_{n}>\frac{10^{5} \cdot \text { PouT }}{1.16 \cdot \Delta B \cdot f \cdot d} \quad=0.143 \mathrm{~cm}^{4}
$$

Eq. 2
where:
Pout = output 15 (W)
$\Delta B=$ flux density swing ( $T$ ) we chose $\Delta B=200 \mathrm{mT}$
d $=$ current density we chose $=450 \mathrm{~A} / \mathrm{cm}^{2}$
$f \quad=$ working frequency of transformer
$A_{e}=$ effective area of magnetic path $\left[\mathrm{cm}^{2}\right]$
$A_{n}=u s e f u l$ winding cross section $\left[\mathrm{cm}^{2}\right]$
The core size is then $E E 25 \times 6.5$ with $A_{e}=0.42 \mathrm{~cm}^{2}$,
$A_{n}=0.45 \mathrm{~cm}^{2}$ and $A_{e} . A_{n}=0.189 \mathrm{~cm}^{4}>0.143 \mathrm{~cm}^{4}$.
The maximum value of primary current at $V_{\text {MIN }}$ is :

$$
\begin{align*}
I P & =\frac{P_{\text {OUT }}}{\eta \cdot \delta_{\text {MAX }} \cdot\left(V_{\text {MIN }}-\Delta \bar{V}\right)} \\
& =\frac{15}{0.75 \cdot 0.8 \cdot 9}=2.8 \mathrm{~A} \tag{Eq. 3}
\end{align*}
$$

where $\Delta V$ is the voltage drop on the $R 9$ resistor and on the POWER MOS, $\delta_{\text {max }}=$ maximum duty cycle, $\eta$ = efficiency.
The turns ratio is given by the following equations:
$n=\frac{V_{\text {prim. }}}{V_{\text {sec }}} \cdot \delta_{\text {max }}$
$n=\frac{V_{\text {MIN }}-\Delta V}{V_{\text {OUT }}+V_{f}} \cdot \delta_{\text {MAX }}=1.03$
Eq. 4
The number of turns $N_{p}$ is calculated as follows :
$N_{p M I N}=\frac{V_{\text {MIN }}[V] \cdot \delta_{\text {MAX }}}{\Delta B[T] \cdot A_{e}\left[\mathrm{~cm}^{2}\right] \cdot f[\mathrm{~Hz}]} \cdot 10^{4}=9.5$ turn
Eq. 5
The number of turns used was $N_{p}=10$ and $N_{s}=10$. The primary inductance is then the same as the secondary inductance.
$L_{p}=L_{s} \doteq N_{p}{ }^{2} \cdot A_{L}=100 \cdot 2400 n H=240 \mu H$
The value of $L_{d}$ (leakage inductance) was measured on the transformer :

$$
L_{d}=0.5 \mu \mathrm{H}
$$

## OUTPUT FILTER

The most interesting part of the output filter is the transformer T2 which, coupling the output series inductance of the two outputs, gives good regulation of the -6 V output (magnetic regulator).
T2 construction is very simple because the two inductance are directly wound on the same cylindrical ferrite core. Each winding is made up of 200 turns and is: $L(+6 \mathrm{~V})=L(-6 \mathrm{~V})=17 \mu \mathrm{H}$.
The four fast recovery diodes used are BYW29-100 type.
Capacitors C10, C11 are $220 \mu \mathrm{~F}$ Roederstein EKR low ESR type for application in switching power supplies.
The ripple value obtained is very low $=50 \mathrm{mV}$ peak to peak (photo 3).

Photo 1 : Tr2, Tr3, $\mathrm{V}_{\mathrm{ds}}\left(\mathrm{V}_{\mathrm{ds}}=20 \mathrm{~V} / \mathrm{div}.\right)$.


Photo 2 : Tr3 Waveforms $\left(V_{G}=10 \mathrm{~V} /\right.$ div, $V_{d s}=20 \mathrm{~V} / \mathrm{div}, \mathrm{l}_{\mathrm{d}}=1 \mathrm{~A} / \mathrm{div}$.).


## COMPONENT LIST

Resistors

| R1 | $=8.2 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| :--- | :--- | :--- |
| R2 | $=5.6 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R3 | $=1.2 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R4 | $=1.5 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R5 | $=1.2 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R6 | $=470 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R7 | $=3.3 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R8 | $=390 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R9 | $=0.22 \Omega$ | 1 W |
| R10 | $=10 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R11 | $=22 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R12 | $=22 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R13 | $=5.6 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R14 | $=5.6 \mathrm{~K}$ | $1 / 4 \mathrm{~W}$ |
| R15 | $=18 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R16 | $=47 \Omega$ | $1 / 4 \mathrm{~W}$ |
| R17 | $=33 \Omega$ | $1 / 2 \mathrm{~W}$ |

Capacitors

| C 1 | $=100 \mu \mathrm{~F}$ |
| :--- | :--- |
| C 2 | $=1 \mathrm{nF}$ |
| C 3 | $=1 \mu \mathrm{~F}$ |
| C 4 | $=10 \mathrm{nF}$ |
| C5 | $=1.8 \mathrm{nF}$ |
| C 6 | $=2.2 \mu \mathrm{~F}$ |
| C 7 | $=10 \mathrm{nF}$ |
| C 8 | $=2.7 \mathrm{nF}$ |
| C 9 | $=10 \mathrm{nF}$ |
| C10 | $=220 \mu \mathrm{~F}$ |
| C11 | $=220 \mu \mathrm{~F}$ |
| C 12 | $=330 \mathrm{nF}$ |
| C13 | $=330 \mathrm{nF}$ |

Transistors
TR1 $=2 \mathrm{~N} 2907$
TR2, TR3 $=$ IRFZ20
Diodes
D1, D2, D3, D4 = BYW2929-100

ICs
$11=$ SGS3525A

## Transformers

T1 core $=$ TOMITAEE $25 \times 6.52$ E6 Material
T2 core $=$ cylindrical $30 \times 20 \mathrm{~mm}$

Photo 2a: Turn On.


Photo 3 : Ripple on +6 V and -6 V Outputs ( $20 \mathrm{mV} / \mathrm{div}$.).


Photo 2b: Turn Off.


Photo 4 : Transient Response ( $20 \mathrm{mV} / \mathrm{div}$.).


