## design ideas

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## LED driver doubles as fault monitor

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EDS FIND WIDE USE as indicators and as light emitters in devices such as optocouplers. In some applications, the LED or the emitter may be located remotely at some distance from the main unit. Typical examples are dashboard-

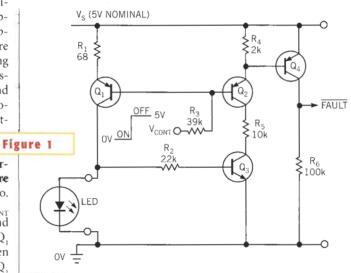
mounted automotive indicators and industrial optosensors. In critical applications, you may require some means of monitoring the integrity of the LED. Using just four transistors and six resistors, this circuit provides switchable, constant-current drive for an

LED and indicates both open- and short-circuit fault conditions (**Figure 1**). And there's a bonus, too. Control signal V<sub>CONT</sub> switches the LED on and off. When V<sub>CONT</sub> is high, Q<sub>1</sub> and the LED are off. When V<sub>CONT</sub> is as low as 0V, Q<sub>1</sub> turns on and sources a constant current to the LED. Because most LEDs have a

forward-voltage drop of at least 1.2V, adequate base-bias voltage exists for  $Q_3$ , which turns on, thereby providing a conduction path for  $Q_2$ . This conduction, in turn, provides bias for  $Q_4$ , which turns on

and pulls high, thus indicating a healthy LED.

Because  $Q_2$  and  $Q_4$  are both now on, the base potential of  $Q_1$  sits at roughly two  $V_{\rm BE}$  drops below the positive-supply rail,  $V_{\rm S}$ , thereby placing one  $V_{\rm BE}$  drop



This LED driver doubles as a fault monitor and limits short-direct current to boof.

across R<sub>1</sub>. Consequently, with R<sub>1</sub>=68 $\Omega$ , Q, sources a steady current of approximately 10 mA to the LED. Provided that the value of R, is large enough, little of the LED's forward current diverts into Q<sub>3</sub>'s base. As long as the LED remains undamaged, FAULT stays high, signaling normal drive conditions. Should the LED go open-circuit, Q,'s collector load becomes just R, in series with Q,'s base. Because R, is much larger than R, Q, saturates, the voltage across R, falls to around 20 mV or so, and the emitter potentials of Q<sub>1</sub> and Q, rise toward V<sub>5</sub>. With insufficient base drive, Q now turns off, and the output falls to 0V to signal the fault condition.

On the other hand, if a fault puts a short circuit across the LED,  $Q_3$  imme-

diately turns off and deprives  $Q_2$  of collector current.  $Q_2$ 's base-emitter junction now behaves like a diode, clamping  $Q_1$ 's base to a potential dictated mainly by  $Q_2$ 's  $V_{BE}$  drop and by the ratio of  $R_3$  to  $R_4$ . Because  $R_4$ 's value is smaller than

that of R<sub>3</sub>, Q<sub>2</sub>'s emitter potential now rises toward V<sub>s</sub>. Once again, Q turns off and goes low to indicate the fault condition. With the resistor values shown in Figure 1, Q,'s base now sits at approximately 4V, leaving only 200 to 300 mV across R<sub>1</sub>. Therefore, the short-circuit current is effectively "choked back" to less than a third of the normal value, thereby saving power-the bonus. Under normal conditions, with the LED on, Q, conducts more current than Q,, causing its V<sub>BE</sub> drop to be slightly larger than that of Q. Consequently, the potential across R, is slightly less than a diode drop, and you

may need to experiment with the value of R, to set the desired LED current.

You must select R, to satisfy the basecurrent requirements of Q, and Q, when  $V_{CONT}$  is low. Tests on the prototype circuit produced good results with R<sub>3</sub>=39  $k\Omega$ , although a smaller value may be required, depending on the LED current and the current gain of Q, and Q,. When the LED is on, both Q, and Q, are fully on, so a reasonably large value of R<sub>5</sub> is required to limit their joint collector current to an acceptable level. However, R<sub>E</sub> must not be too large, or Q, will be unable to furnish the current that R, and Q<sub>1</sub>'s base require. Making R<sub>2</sub> approximately four or five times larger than R is a good starting point.

Although the circuit in Figure 1 has a

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5V supply, you could use other voltages, provided that you scale the resistor values accordingly. Operation at lower voltages is possible as long as  $Q_1$  has adequate "headroom" to stay out of

saturation, but beware of problems if you use a blue or a white LED, because these devices tend to have relatively high forward-voltage drops. The transistor types are not critical; most small-signal devices with high current gain should be adequate, although Q<sub>1</sub> may need to be a power device if your design requires a high LED current, a high supply voltage, or both.