## Novel circuit isolates temperature sensor from its host

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Temperature sensors must sometimes operate at locations whose return potentials differ considerably from that of the data-acquisition system's common—that is, equipotential—ground. In consequence, the temperature sensor's support circuitry must provide galvanic isolation between the sensor and its data-acquisition system. Also, the data-acquisition system seldom provides an isolated source of power for the sensor. The circuit in **Figure 1** solves both problems by isolating the sensor's signal and power supply.

The complementary, fixed-frequency square-wave outputs of a power-transformer driver— $IC_1$ , a Maxim (www. maxim-ic.com) MAX845—drive a Halo

Electronics (www.haloelectronics.com) TGM-010P3 1-to-1-to-1 transformer with dual primary windings and a single untapped secondary winding (Reference 1). The secondary winding feeds a Graetz-bridge rectifier that generates approximately 4.5V to power IC<sub>2</sub>, a Maxim MAX6576 sensor. Combining a temperature sensor, signal-processing electronics, and an easy-to-use digital-I/O interface in a low-cost package, the MAX6576 draws little current from a single supply source and maintains its specified accuracy over a 3 to 5V supply-voltage range.

## designideas



Figure 1 Transformer T<sub>1</sub> isolates the temperature sensor,  $IC_{2^1}$  from the equipment under test. The period of IC<sub>1</sub>'s digital output varies as a function of temperature. The circuit's output period varies at a rate of 10  $\mu$ sec/°K. User-selected scale factors range from 10 to 640  $\mu$ sec/°K.





When  $Q_2$  conducts, it draws an asymmetrical power-supply current that exceeds the supply current during the sensor output's positive half-cycle.

In IC<sub>1</sub>'s sensor output-to-ground return on the data-acquisition system's side, resistor R<sub>2</sub> and capacitor C<sub>2</sub> shunt Q<sub>1</sub>'s base-emitter junction. The values of R<sub>2</sub> and C<sub>2</sub> ensure that the sum of IC<sub>2</sub>'s current and transformer T<sub>1</sub>'s magnetizing current cannot drive Q<sub>1</sub> into conduction. When Q<sub>2</sub> conducts, it draws about 12 mA from the isolated 4.5V power-supply line. Reflecting to the primary, Q<sub>2</sub>'s conduction current flows from the 5V supply into IC<sub>1</sub>, out through its ground terminals, and partly through R<sub>2</sub>. The voltage drop across  $R_2$  exceeds  $Q_1$ 's base-emitter voltage threshold and supplies sufficient base current to turn on  $Q_1$ .

Thus, when  $Q_2$  conducts, so does  $Q_1$ , which copies IC<sub>1</sub>'s isolated square-wave output to  $Q_1$ 's collector circuit. As the waveforms of **figures 2** and 3 show,  $Q_1$ 's output rise and fall times, jitter, and propagation delay total about 2 µsec. The equivalent measurement error due to timing jitter amounts to less than 0.1°K at the fastest conversion constant of 10 µsec/°K. Varying the circuit's supply voltage through a range of 4.5 to 5.5V introduces an error of less than 0.1°K. The output at  $Q_1$ 's collector can sink several milliamperes at a voltage excursion of 0 to 5V.



## designideas

This design can accommodate temperature-to-frequency converters and other types of temperature sensors. For further information on  $IC_1$  and  $IC_2$ , review the devices' data sheets and the data sheet for the MAX845 evaluation kit (references 2, 3, and 4).EDN

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