## Audio-test accessory isolates and matches loads

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Connecting a $600 \Omega$ audio circuit to a 50 or $75 \Omega$ circuit or test instrument requires an impedancematching circuit or, when isolation of the circuits is necessary, a transformer. Both approaches offer advantages and disadvantages. A conventional transformer can match impedances with low typical losses of 1.5 dB , provide dc isolation, and operate from either a balanced or an unbalanced, $600 \Omega$ primary circuit. A high-quality transformer's pass-
band can accommodate an audio-frequency range of 300 Hz to 15 kHz with minimal amplitude variation. However, transformers that can match 600 to 50 or $75 \Omega$ may not be readily available or may command a cost premium.

A minimum-loss, fixed-value im-pedance-matching circuit, or pad, provides frequency-invariant audio-impedance transformation and can comprise as few as two resistors. Although a pad can provide useful impedance

| TABLE 1 INSERTION LOSS VERSUS FREQUENCY |  |  |
| :---: | :---: | :---: |
| Frequency | Insertion loss (dB) | Insertion loss (dB) |
| $(\mathrm{kHz})$ | 600 to $50 \Omega$ | 600 to $75 \Omega$ |
| 0.1 | 11.7 | 8.7 |
| 0.3 | 10 | 7 |
| 0.5 | 9.5 | 6.7 |
| 1 | 9.2 | 6.5 |
| 2 | 9 | 6.3 |
| 5 | 8.9 | 6.1 |
| 10 | 8.8 | 6.1 |
| 20 | 8.8 | 6 |
| 50 | 8.9 | 6.1 |
| 100 | 9.5 | 6.7 |



COAXIAL CONNECTORS $J_{1}$, $J_{2}$, AND $J_{3}$ ARE AMPHENOL PART NO. 31-10-RFX.
IF MECHANICAL COMPATIBILITY WITH $75 \Omega$ BNC SERIES CONNECTORS IS NECESSARY, REPLACE $J_{3}$ WITH AN APPROPRIATE CONNECTOR.

Figure 1 A handful of passive components creates a handy test fixture for matching impedances in audio-test circuits.

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matching, it introduces a significant insertion loss of 14.8 dB for a 600 -to$75 \Omega$ transformation or 16.6 dB for a 600 -to- $50 \Omega$ transformation, either of which might impose an unacceptable loss of dynamic range.
Part of a suite of test accessories, this low-cost, switchable, dual-impedance transformation circuit comprises a single conventional transformer and two minimum-loss pads (Reference 1). A single inexpensive, conventional transformer steps down the $600 \Omega$ primary input impedance to an intermediate impedance level of $100 \Omega$ (Figure 1). Switch $S_{1}$ selects a 100 to $50 \Omega$ or a 100 to $75 \Omega$ minimum-loss pad. Construction of the unit involves noncritical point-to-point wiring, although this design uses a Hammond 1590LB die-cast-aluminum box to provide shielding and a rugged enclosure to support three Amphenol (www.amphenolrf. com) RFX series BNC panel-mounted, insulated-frame input and output jacks. $\mathrm{T}_{1}$ is a Mouser Electronics (www.mouser.com) 42TM031 audio transformer, and the resistors are 0.5 W , metal-film units with $\pm 1 \%$ tolerances. With quantity discounts, the overall bill-of-materials cost is less than $\$ 20$.
To verify frequency response and


## designideas

attenuation in a $600 \Omega$ test setup, connect two identical units back to back through their 50 or $75 \Omega$ terminals. You obtain the measured data (Table 1) for a single unit by halving the 600 -to$600 \Omega$ transmission-loss measurements.

Calculated insertion loss for the 100 to $50 \Omega$ minimum-loss pad is 7.7 dB , and insertion loss for the 100 to $75 \Omega$ mini-mum-loss pad is 4.8 dB . Subtracting these values from the measured losses indicates that the transformer con-
tributes a midband loss of 1.3 to 1.5 dB . Insertion loss due to stray coupling from the selected output port to an unused output exceeds 40 dB . Combining a conventional transformer with two minimum-loss pads takes advantage of the best of both techniques.
The low-cost transformer contributes moderate insertion losses and provides dc isolation and good frequency response. In addition, the transformer's low-frequency roll-off
helps reduce $60-\mathrm{Hz}$ hum and low-frequency noise. The electrically isolated input jack allows connection of the transformer's input to balanced or grounded $600 \Omega$ sources.EDN

## REFERENCE

IT Kurzrok, Richard M, "Simple LabBuilt Test Accessories for RF, IF,
Baseband, and Audio," High Frequency Electronics, May 2003, pg 60.

