Paraphase Tone Control



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As opposed to the widespread Baxandall circuit (dating back to 1952!) a 'paraphrase' tone control supplies a straight frequency response as long as the bass and treble controls are in the same position. This unique property makes the 'paraphase' configuration of interest if *only* treble or bass needs to be adjusted — it is not possible to adjust both at the same time! Essentially, it's the difference in setting of the tone controls that determines the slope of the frequency response, and the degree of bass/treble correction.

The circuit in **Figure 1** is simplicity itself, based on two networks C1-C2-C3/R9-R10-R11 and C5-C6-C7/R12-R13-R14. The first is for the high frequencies (treble) response, the second, for the low frequencies (bass). The roll-off points have been selected, in combination with C4 and C8, for the sum of the two output signals to re-appear with a 'straight' frequency response again at the output. Roughly equal output levels from the networks are ensured by R6 = 7.15 k Ω and R8 = 6.80 k Ω . However, the operating principle requires the input signals to the two networks to be in anti-phase.

For best operation the networks are driven by two buffers providing some extra gain. The gain of IC1.D is slightly



Specification

Current consumption (no signal)		8 mA
Max. input signal		1 V _{eff} (at max. gain)
Gain	at 20 Hz	+13.1 dB max. –6.9 dB min.
	at 20 kHz	+12.2 dB max. -7.6 dB min
Gain (controls at mid position)		2.38 x
Distortion (1 V _{eff} , 1 kHz)		0.002% (B = 22kHz) 0.005% (B = 80 kHz)



higher than that of IC1.C to ensure the overall response curve remains as flat as possible at equal settings of the tone controls. Because each network introduces a loss of about 1.72 (times), IC1.D and IC1.C first amplify the signal. The gain is set at about 8 (times) allowing input signal levels up to 1 V to pass the circuit at maximum gain and distortion-free. The gain also compensates the attenuation if you prefer to keep the tone controls at the

COMPONENTS LIST

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Resistors
\begin{array}{l} \mathsf{R1}\text{-}\mathsf{R4} = 10\mathsf{k}\Omega\\ \mathsf{R5}\text{,}\mathsf{R7} = 1\mathsf{k}\Omega \end{array}
R6 = 7k\Omega 15
R8 = 6k\Omega 80
R9,R10,R11 = 8k\Omega 2
R12, R13, R14 = 2k\Omega 2
R15 = 1M\Omega
R16 = 100\Omega
R17 = 100k\Omega
P1,P2 = 100k\Omega preset or chassis-
  mount control potentiometer, linear
  law
Capacitors
C1,C2,C3 = 47nF MKT, lead pitch
  5mm
C4 = 68nF MKT, lead pitch 5mm
C5,C6,C7 = 10nF MKT, lead pitch
  5mm
C8,C10,C11 = 100nF MKT, lead
pitch 5mm
C9 = 2µF2 MKT, lead pitch 5mm or
  7.5mm
Semiconductors
IC1 = TL074
Miscellaneous
K1,K2 = line socket, PCB mount, e.g.
  T-709G (Monacor/Monarch)
PCB, ref. 060015-1 from The
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mid positions for a straight response. To audio fans, the circuit is rewarding to experiment with, especially in respect of the crossover point of the two networks. R3 and R4 determine the control range, which may be increased (within limits) by using lower resistor values here. The values shown ensure a tone control range of about 20 dB.

IC1.B buffers the summed signal across





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R15. C9 removes any DC-offset voltage and R16 protects the output buffer from the effects of too high capacitive loads. R17, finally, keeps the output at 0 V. The choice of the quad opamp is relatively uncritical. Here the unassuming TL074 is used but you may even apply rail to rail opamps as long as they are stable at unity gain. Also, watch the supply voltage range.

The graph in **Figure 2** (produced by our Audio Precision analyser) shows nine response curves obtained by setting the two tone controls to minimum, mid position and maximum. Note that 0 dB is relative to the mid position of the pots! A simple circuit board was designed for the project (**Figure 3**). Linear-law potentiometers may be fitted directly onto the board. Two boards are required for a stereo application. The relevant connections on the boards are then wired to a stereo control potentiometer.

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