# Paraphase Tone Control 



## Ton Giesberts

As opposed to the widespread Baxandall circuit (dating back to 1952!) a 'paraphrase' tone control supplies a straight frequency response as long as the bass and treble controls are in the same position. This unique property makes the 'paraphase' configuration of interest if only treble or bass needs to be adjusted - it is not possible to adjust both at the same time! Essentially, it's the difference in setting of the tone controls that determines the slope of the frequency response, and the degree of bass/treble correction.

The circuit in Figure 1 is simplicity itself, based on two networks C1-C2-C3/R9-R10-R1 1 and C5-C6-C7/R12-R13-R14. The first is for the high frequencies (treble) response, the second, for the low frequencies (bass). The roll-off points have been selected, in combination with C4 and C8, for the sum of the two output signals to re-appear with a 'straight' frequency response again at the output. Roughly equal output levels from the networks are ensured by $\mathrm{R} 6=7.15 \mathrm{k} \Omega$ and $R 8=6.80 \mathrm{k} \Omega$. However, the operating principle requires the input signals to the two networks to be in anti-phase.
For best operation the networks are driven by two buffers providing some extra gain. The gain of IC1.D is slightly


higher than that of IC I.C to ensure the overall response curve remains as flat as possible at equal settings of the tone controls. Because each network introduces a loss of about 1.72 (times), ICI.D and ICI.C first amplify the signal. The gain is set at about 8 (times) allowing input signal levels up to 1 V to pass the circuit at maximum gain and distortion-free. The gain also compensates the attenuation if you prefer to keep the tone controls at the

[^0]mid positions for a straight response. To audio fans, the circuit is rewarding to experiment with, especially in respect of the crossover point of the two networks. R3 and R4 determine the control range,
which may be increased (within limits) by using lower resistor values here. The valves shown ensure a tone control range of about 20 dB .
IC1.B buffers the summed signal across



R15. C9 removes any DC-offset voltage and R16 protects the output buffer from the effects of too high capacitive loads. R17, finally, keeps the output at 0 V . The choice of the quad opamp is relatively uncritical. Here the unassuming TLO74 is used but you may even apply rail to rail opamps as long as they are
stable at unity gain. Also, watch the supply voltage range.
The graph in Figure 2 (produced by our Audio Precision analyser) shows nine response curves obtained by setting the two tone controls to minimum, mid position and maximum. Note that 0 dB is relative to the mid position of the pots!

A simple circuit board was designed for the project (Figure 3). Linear-law potentiometers may be fitted directly onto the board. Two boards are required for a stereo application. The relevant connections on the boards are then wired to a stereo control potentiometer.
(060015-1)


[^0]:    COMPONENTS LIST

    Resistors
    R1-R4 $=10 \mathrm{k} \Omega$
    $R 5, R 7=1 \mathrm{k} \Omega$
    $\mathrm{R} 6=7 \mathrm{k} \Omega 15$
    $\mathrm{R} 8=6 \mathrm{k} \Omega 80$
    $\mathrm{R} 9, \mathrm{R} 10, \mathrm{R} 11=8 \mathrm{k} \Omega 2$
    R12,R13,R14 = $2 \mathrm{k} \Omega 2$
    $R 15=1 M \Omega$
    $\mathrm{R} 16=100 \Omega$
    $\mathrm{R} 17=100 \mathrm{k} \Omega$
    P1,P2 $=100 \mathrm{k} \Omega$ preset or chassismount control potentiometer, linear law

    ## Capacitors

    C1,C2,C3 $=47 \mathrm{nF}$ MKT, lead pitch
    5 mm

    - $\mathrm{C} 4=68 \mathrm{nF}$ MKT, lead pitch 5 mm

    C5,C6,C7 = 10 nF MKT, lead pitch 5 mm
    C8,C10,C11 = 100nF MKT, lead pitch 5 mm
    $\mathrm{C} 9=2 \mu \mathrm{~F} 2 \mathrm{MKT}$, lead pitch 5 mm or
    7.5 mm

    Semiconductors
    $\mathrm{ICl}=\mathrm{TLO74}$

    ## Miscellaneous

    K1,K2 = line socket, PCB mount, e.g. T-709G (Monacor/Monarch)
    PCB, ref. 060015-1 from The PCBShop

